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# Twist- and Supertwist Antidazzling Devices With Local Reduction of Brightness

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TWIST- AND SUPERTWIST ANTIDAZZLING DEVICES WITH LOCAL REDUCTION OF BRIGHTNESS

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ABSTRACT. Single- and multichannel optoelectronic modulators with twist- and supertwist transmissive or reflective LC cells are described. The possibility of antidazzling aplications of these devices at low background intensity (0, 1-10 lx) is discussed.

#### INTRODUCTION.

The liquid crystalline shutters may reduce beam by a factor tens and more during a short time interval Ιt (0.1-10)13 especially useful ms). to eliminate the applications. blindeness of an operator in many paper we describe the design and controlling regime of two Οf antiglare modulators With total reduction of brigtness of a dazzling light source.

first one 13 single-channel optoelectronic with threshold dependence ٥f transmission on input light intensity. This device provides reduction of brightness. The second one optically addressed spatial light modulator (OA consists of an aggregate shutters with of optoelectronic the threshold input-output intensity characteristics. These shutters interact very weak due to low diffusion of charge carriers in Photosensitive part Οf а SLM. The threshold input-output character1st1c provides ٥f intensity only ٥f very bright parts of an For antiglare applications twistimage transformed. supertwist shutters may be useful. Automative light sunglasses are described in Ref. i. The a-Si solar control two battery controls the transmission ٥f twist-cells 1 n intensities range 1000-20000 lx. Obviously these glasses may not operate at 10W illuminance level antiglare device. The local reduction of bright parts of described Refs. 2, 3, The SLMs image 13 ın "photoconductor - liquid crystal" (PC-LC) were used. comparison with metal dielectric -Slow in ones are crystal" (MDS-LC) semiconductor - liquid structures which operate usually in a reflective mode. The purpose ٥f the single - and 13 the design

optoelectronic antiglare device with total or local reduction of light beam which operate at relative low intensity level (0, 1-10 lx).

## 2. TWIST ELECTROOPTIC SHUTTER FOR ANTIGLARE SPECTACLES.

The problems of road visibility under highway conditions occupy a special position in traffic safety. Up to 15% of all accidents take place in conditions of limited visibility on the average [4]. One of the main reasons for traffic accidents is that the upper beam of head lamps of the oncoming vehicles dazzles a driver. To eliminate the dazzling effect it is necessary to reduce the luminous flux by the factor of 10-50.

This paper describes device that prevents blinding the driver by the distant beam of head lights of The device consists of two electrooptical crystalline shutters (twist cells), the goggles frame and of electronic control circuit, allowing to vary the transmission of the shutters. as the illuminance of Photodetector varies. The design of the device is presented Fig. 1. The electronic control circuit comprises a square-wave generator of monopolar pulses. A Photodiode in the supply circuit of the generator, which shuts off the voltage in the case of absence cell's blas exposure.

The thickness of the liquid crystal material layer specified in accordance with the condition of the second For liquid crystalline material Gooch-Tarri maximum [5]. ZhK-1282, having the birefringence value  $\triangle$  n = 0,14 , the thickness of the layer L is  $\Lambda\sqrt{15/2}\Delta$  n, i.e. L = 12,6 M m. if  $\lambda = 0.55 \,\text{M}$  m. To provide the uniform twist of the LC layer the chiral dopant is introduced into the material from to with a concentration chosen condition the C<0,25A/L, where A is the twisting ability of the

Now we describe the method of the operating device. threshold value of the dazzling 111umination driver's eyes is equal to 1.4 - 2 luxes according to [4]. When the Photodetector illumination exceeds this value, the control curcuit generates a consequence οf monopolar voltage pulses into the electrooptical shutters. the transmission ٥f liquid crystal decreases 40 50 When times. the input decreases up to the level below the threshold value. control curcuit shuts off the generator

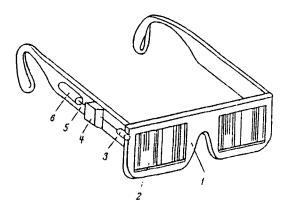


Fig. 1. Design of antiglare device: 1 - frame, 2 - electro - optic shitters (twist cells), 3 - photodetector, 4 - modulator (electronic key), 5 - wires, 6 - battery (or generator)

orientation relaxes into the initial position and the shutter is open. In the case of full reorientation of the liquid crystal the width of angular dependence is inversely proportional to the product of optical anisotropy and thickness of the liquid crystal layer. The half-width of angular dependence was 0.5 rad at the thickness of ZhK-i282 12 Mm.

Under these conditions an appreciable attenuation of the distant light of oncoming traffic and small attenuation of close light of a driving car take place[6]. The use of antidazzling spectacles by drivers of transport vehicles in conditions of darkness enables the drivers to adapt to distant and close headlight beams what leads to reduction of eye's accommodation time, and increases the safety of driving.

# 3. SUPERTWIST REFLECTIVE SPATIAL LIGHT MODULATOR WITH LOCAL REDUCTION OF A BRIGHT LIGHT SOURCE

photosensitive and SLM consists Οf Any which are distanced by a dielectric parts modulating mirror. The first one is the MDS-structure (ITO electrode optical glue - GaAs plate 50 m thick). The dielectric mirror reflects the visible range of spectrum and transmits the IR one. Therefore, we use the infrared beam to write an image on the MDS and the visible beam to read the image transformed. The electrooptic layer is a planar oriented twisted nematic LC. The twist angle  $\gamma = 63.6$  (2m+1) (m - an integer) and optical phase retardation  $\Delta nL = (\lambda 2 \sqrt{2})(2m+1)$ 

(An - LC birefringence, L - LC layer thickness, A - read light wave length) are chosen from [7,8] to transform a linear polarization into a circular one. When a LC layer is not deformed by the electric field the output after by the electric field the output polarization is perpendicular to the input one after the reflection. The deformed LC layer does not change the polarization of a read light beam. The electrooptics of such cells was investigated in Ref. 9.

The twist angle 🌱 =191° provided steeper voltage transmission characteristics and higher photosensibility of SLM. The value of △n low = 0,045 requirement to the LC layer thickness homogeneity. The 13 light beam transformed bУ the SLM without a The similar sinificant colouring. design of the LC layer were used in Ref. 10 in an a-Si SLM.

The experimental scheme 18 shown in F1g. 2. objective O<sub>1</sub> projects an image of low-angle bright source on the semiconductor surface. The polarizing light d ivider C transformes the Phase-modulated read-beam into the amplitude-modulated one and guides it on ocular O2 before the operator's eye.

The input-output intensity characteristics is shown in F1g. 3. The flat interval ٥f Iout (Iin) dependence corresponds the absence of variation of intensity transformed image when the input intensity increases, the reduction of brightness of a light source relative to the background intensity. The threshold intensity Ith and reduction coefficients Kred may be controlled by the variation of driving parameters: voltage U and frequency f. Ith value increases too and Knod When f increases the steepness of diminishes. The Iout(Iin) characteristics depends strongly on a ratio ٥f thicknesses of LC and dielectric layers and on LC parameters, such as dielectric anisotropy and elastic constants ratio [11,12].

The real value of Krad of white light beam was 10-30 at In = 100-1000 lx. It is necessary to enlarge this value and use additive electrooptic shutter for welding applications.

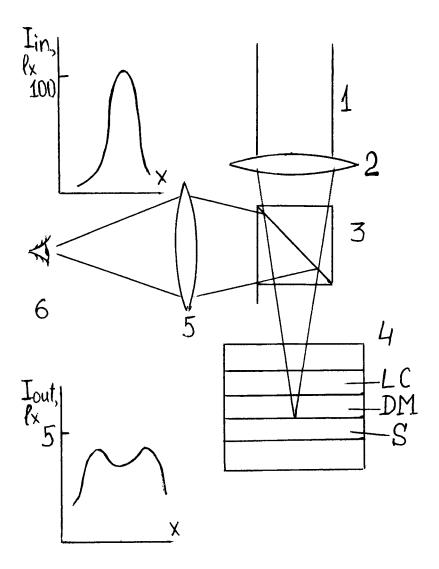


Fig. 2. Scheme of measurement of parameters of local brightness reduction. i - input light beam, 2 - objective Oi, 3 - light - divider, 4 - SLM (LC - liquid cristal, DM - dielectric mirror, 5 - semiconductor layers), 5 - ocular O2, 6 - observer's eye or photodetector. Iin and Iout light beams are also shown.

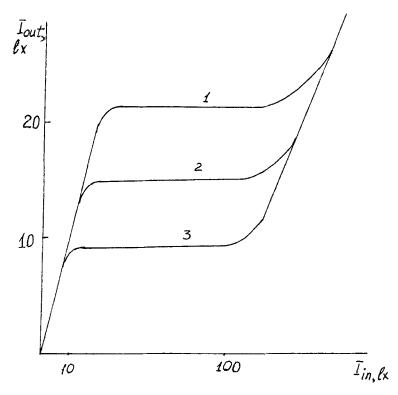


Fig. 3. The dependence of output image intensity Iout on input intensity Iin at supply frequencies 5 (1), 1 (2), 0, 1 (3) kHz.

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